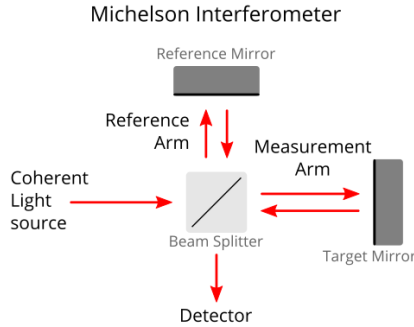


## INTRODUCTION

A Michelson interferometer, probably the most popular interferometer architecture, is schematically drawn in Figure 1.



**Figure 1.** Basic setup of a Michelson interferometer.

A coherent light source (laser) is split at a beam splitter into a reference and a measurement arm. Both partial beams are reflected at a reference and target mirror, respectively, and recombine at the beam splitter, forming interferences. The interference signal  $I(t)$  measured at the detector can be written as:

$$I(t) = \cos\left(\frac{4\pi}{\lambda} \cdot x(t)\right) \quad (1)$$

where  $\lambda$  is the laser wavelength and  $x(t)$  is the length difference between reference and measurement arms.

## WAVELENGTH MODULATION

A wavelength modulation of the laser source, by electronically modulating the injection current of appropriate laser diodes for instance<sup>1</sup>, can be expressed as:

$$\lambda = \lambda(t) = \lambda_0 + \delta\lambda(t) = \lambda_0 + \delta\lambda \cdot \sin(\omega t), \quad (2)$$

where  $\lambda_0$  is the carrier wavelength and  $\omega/2\pi$  is the modulation frequency.

For practical reasons,  $\delta\lambda \ll \lambda_0$  and Equation 2 can be rewritten such that:

$$\frac{1}{\lambda(t)} = \frac{1}{\lambda_0 + \delta\lambda(t)} \approx \frac{1}{\lambda_0} \cdot \left(1 - \frac{\delta\lambda \cdot \sin(\omega t)}{\lambda_0}\right). \quad (3)$$

Equation 1 becomes:

$$I(t) \approx \cos\left(\frac{4\pi}{\lambda_0} \cdot x(t) - \frac{4\pi}{\lambda_0^2} \cdot \delta\lambda \cdot x(t) \cdot \sin(\omega t)\right) \quad (4)$$

$$\approx \cos(\alpha(t) + z(t) \cdot \sin(\omega t)),$$

<sup>1</sup>For the PICO SCALE Interferometer,  $\lambda_0 = 1550$  nm,  $\delta\lambda < 15$  pm, and  $\omega/2\pi = 30$  MHz

where  $\alpha(t) = \frac{4\pi}{\lambda_0} \cdot x(t)$  is a phase offset which is independent from the modulation frequency and  $z(t) = -\frac{4\pi}{\lambda_0^2} \cdot \delta\lambda \cdot x(t)$  is the modulation depth.

## QUADRATURE DETECTION

Equation 4 can be expanded in terms of Bessel functions using the Jacobi-Anger expansion, which yields:

$$I(t) \propto S_\omega \cdot \cos(\omega t) + S_{2\omega} \cdot \sin(2\omega t) + S_{3\omega} \cdot \cos(3\omega t) + O[\sin(4\omega t)], \quad (5)$$

with

$$S_\omega(t) \propto J_1(z(t)) \cdot \sin(\alpha(t))$$

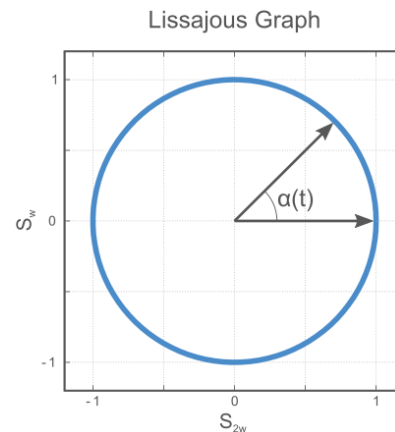
$$S_{2\omega}(t) \propto J_2(z(t)) \cdot \cos(\alpha(t)) \quad (6)$$

$$S_{3\omega}(t) \propto J_3(z(t)) \cdot \sin(\alpha(t))$$

where  $J_n$  are the  $n$ -th Bessel functions of the first kind.

By lock-in filtering  $I(t)$  at frequencies  $n \cdot \omega$  it is possible to obtain the coefficients  $S_{n \in \{1,2,3,\dots\} \cdot \omega}$ . It is clear that consecutive orders differ in phase by 90°, or said to be **in quadrature**, as for the pairs  $(S_\omega; S_{2\omega})$  or  $(S_{2\omega}; S_{3\omega})$ .

When signals in quadrature are plotted against each other, it forms a Lissajous graph, see Figure 2.



**Figure 2.** The pair  $(S_\omega; S_{2\omega})$ , normalized to unity, plotted in a Lissajous graph. The phase  $\alpha(t)$  is directly proportional to the displacement  $x(t)$ .

When the differential arm length changes, for instance when the target mirror moves, it results in the vector representation of the pair in quadrature moving along a circle. The phase  $\alpha(t)$  gives the fraction of one interferometer fringe and by counting full revolutions, macroscopic motions are tracked. Additionally, the direction of motion is revealed. If the distance increases,

the vector rotates clockwise, if the distance decreases, the vector rotates counter-clockwise.

In summary, quadrature detection allows to track macroscopic motions with microscopic resolution - including the direction.

For more information on the technique, there exist many scientific publications, for example [1, 2].

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- [2] Takamasa Suzuki, Mineki Matsuda, Osami Sasaki, and Takeo Maruyama. Laser-diode interferometer with a photothermal modulation. *Applied Optics*, 38(34):7069, dec 1999.

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